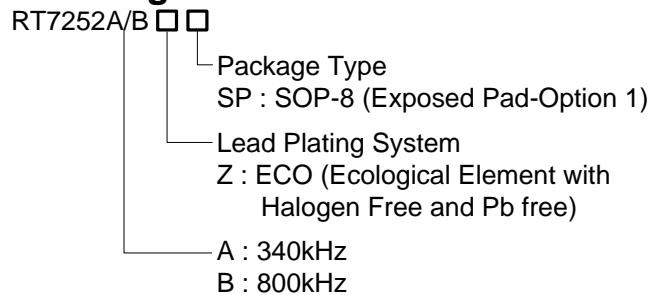


## 2A, 17V, 340/800kHz Synchronous Step-Down Converter

### General Description

The RT7252A/B is a high efficiency, monolithic synchronous step-down DC-DC converter that can operate at 340kHz/800kHz, while delivering up to 2A output current from a 4V to 17V input supply. The RT7252A/B's current mode architecture allows the transient response to be optimized. Cycle-by-cycle current limit provides protection against shorted outputs and soft-start eliminates input current surge during start-up. Fault conditions also include output under voltage protection, output over voltage protection and thermal shutdown. The low current (<5 $\mu$ A) shutdown mode provides output disconnection, enabling easy power management in battery-powered systems. The RT7252A/B is available in a SOP-8 (Exposed Pad) package.

### Ordering Information



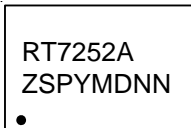
Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

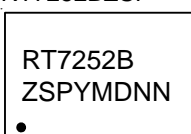
### Marking Information

RT7252AZSP



RT7252AZSP : Product Number  
YMDNN : Date Code

RT7252BZSP



RT7252BZSP : Product Number  
YMDNN : Date Code

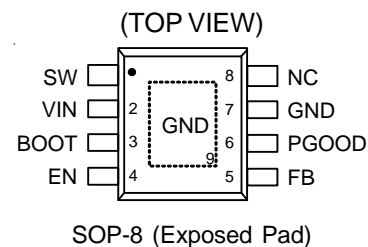
### Features

- 4V to 17V Input Voltage Range
- 2A Output Current
- Internal N-MOSFETs
- Current Mode Control
- Fixed Frequency Operation : 340kHz/800kHz
- Output Adjustable from 0.8V to 12V
- Up to 95% Efficiency
- Internal Compensation
- Stable with Low ESR Ceramic Output Capacitors
- Cycle-by-Cycle Over Current Protection
- Input Under Voltage Lockout
- Output Under Voltage Protection
- Output Over Voltage Protection
- Power Good Indicator
- Thermal Shutdown Protection
- RoHS Compliant and Halogen Free

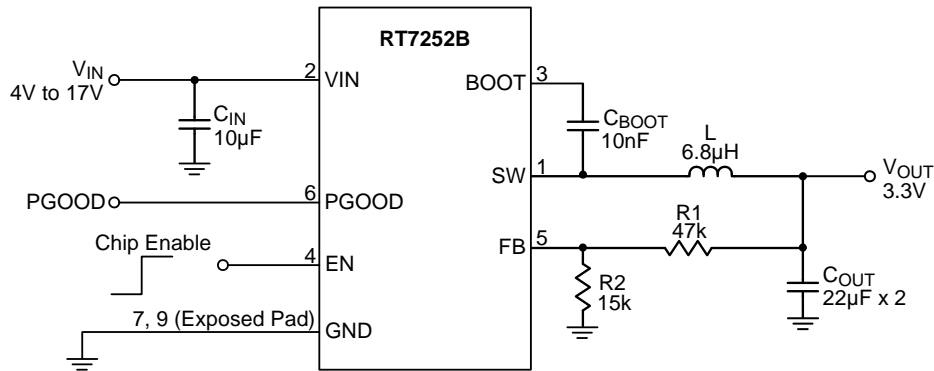
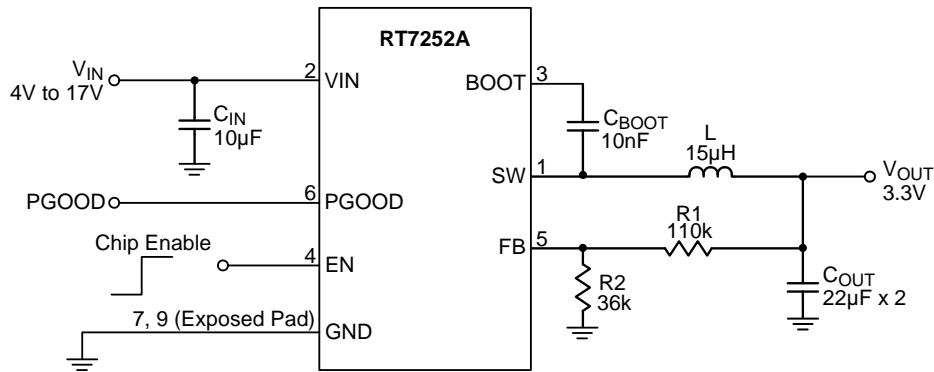
### Applications

- Industrial and Commercial Low Power Systems
- Computer Peripherals
- LCD Monitors and TVs
- Green Electronics/Appliances
- Point of Load Regulation for High-Performance DSPs, FPGAs, and ASICs

### Pin Configuration



## Typical Application Circuit



**Table 1. Recommended Component Selection**

**RT7252A**

V <sub>OUT</sub> (V)	L (µH)	R1 (kΩ)	R2 (kΩ)	C <sub>OUT</sub> (µF)
1.2	4.7	110	220	22 x 2
2.5	10	110	51	22 x 2
3.3	15	110	36	22 x 2
5	22	120	22	22 x 2

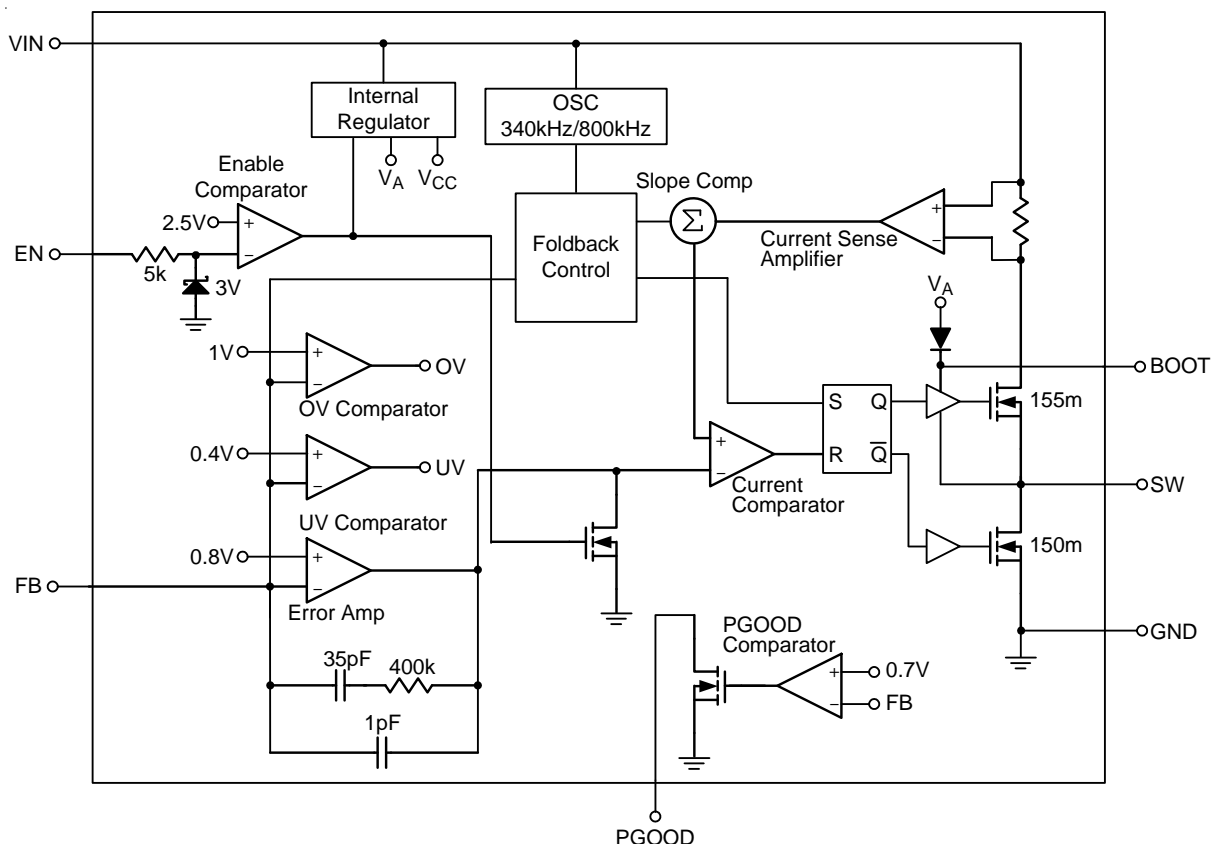
**RT7252B**

V <sub>OUT</sub> (V)	L (µH)	R1 (kΩ)	R2 (kΩ)	C <sub>OUT</sub> (µF)
1.2	3.6	47	91	22 x 2
2.5	4.7	47	22	22 x 2
3.3	6.8	47	15	22 x 2
5	10	62	12	22 x 2

**Functional Pin Description**

Pin No.	Pin Name	Pin Function
1	SW	Switch node. Connect to external L-C filter.
2	VIN	Input supply voltage. Must bypass with a suitably large ceramic capacitor.
3	BOOT	Bootstrap for high side gate driver. Connect 0.01 $\mu$ F or greater ceramic capacitor from BOOT to SW pin.
4	EN	Chip enable. A logic-high enables the converter; a logic-low forces the RT7252A/B into shutdown mode, reducing the supply current to less than 5 $\mu$ A. Attach this pin to VIN with a 100k $\Omega$ pull up resistor for automatic startup.
5	FB	Feedback input pin. For an adjustable output, connect an external resistive voltage divider to this pin.
6	PGOOD	Power good indicator with open drain. The output of this pin is pulled to low when the FB is lower than 0.7V; otherwise it is high impedance. A 100k $\Omega$ pull-high resistor is needed.
7, 9 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
8	NC	No internal connection.

**Functional Block Diagram**



## Absolute Maximum Ratings (Note 1)

- Supply Voltage,  $V_{IN}$  ----- -0.3V to 19V
- SW ----- -0.3V to ( $V_{IN} + 0.3V$ )
- BOOT ----- ( $SW - 0.3V$ ) to ( $SW + 0.3V$ )
- All Other Pins ----- -0.3V to 6V
- Power Dissipation,  $P_D$  @  $T_A = 25^\circ C$   
 SOP-8 (Exposed Pad) ----- 1.333W
- Package Thermal Resistance (Note 2)  
 SOP-8 (Exposed Pad),  $\theta_{JA}$  -----  $75^\circ C/W$   
 SOP-8 (Exposed Pad),  $\theta_{JC}$  -----  $15^\circ C/W$
- Lead Temperature (Soldering, 10 sec.) -----  $260^\circ C$
- Junction Temperature -----  $150^\circ C$
- Storage Temperature Range -----  $-65^\circ C$  to  $150^\circ C$
- ESD Susceptibility (Note 3)  
 HBM (Human Body Model) ----- 2kV  
 MM (Machine Model) ----- 200V

## Recommended Operating Conditions (Note 4)

- Supply Input Voltage,  $V_{IN}$  ----- 4V to 17V
- Junction Temperature Range -----  $-40^\circ C$  to  $125^\circ C$
- Ambient Temperature Range -----  $-40^\circ C$  to  $85^\circ C$

## Electrical Characteristics

( $V_{IN} = 12V$ ,  $T_A = 25^\circ C$ , unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Shutdown Supply Current	I <sub>SHDN</sub>	$V_{EN} = 0V$	--	1	5	$\mu A$
Supply Current	I <sub>OUT</sub>	$V_{EN} = 3V$ , $V_{FB} = 0.9V$	--	0.6	1	mA
Feedback Voltage	$V_{FB}$	$4V \leq V_{IN} \leq 17V$	0.788	0.8	0.812	V
Feedback Current	I <sub>FB</sub>	$V_{FB} = 0.8V$	--	10	--	nA
High Side Switch On Resistance	$R_{DS(ON)1}$		--	155	--	m $\Omega$
Low Side Switch On Resistance	$R_{DS(ON)2}$		--	150	--	m $\Omega$
Upper Switch Current Limit		Min. duty cycle, $V_{BOOT} - V_{SW} = 4.8V$ maximum loading = 2A	--	3.6	--	A
Lower Switch Current Limit		From drain to source	--	1	--	A
Oscillation Frequency	$f_{OSC1}$	For RT7252A	300	340	380	kHz
		For RT7252B	700	800	900	
Short-Circuit Oscillation Frequency	$f_{OSC2}$	$V_{FB} = 0V$ , For RT7252A	--	95	--	kHz
		$V_{FB} = 0V$ , For RT7252B	--	170	--	
Maximum Duty Cycle	$D_{MAX}$	$V_{FB} = 0.7V$ , For RT7252A	--	93	--	%
		$V_{FB} = 0.7V$ , For RT7252B	--	84	--	

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
Minimum On-Time		t <sub>ON</sub>		--	100	--	ns
Input Under Voltage Lockout Threshold		V <sub>UVLO</sub>		--	3.5	--	V
Input Under Voltage Lockout Threshold Hysteresis		ΔV <sub>UVLO</sub>		--	200	--	mV
EN Threshold Voltage	Logic-High	V <sub>IH</sub>		2.7	--	--	V
	Logic-Low	V <sub>IL</sub>		--	--	0.4	
EN Pull Low Current			V <sub>EN</sub> = 2V, V <sub>FB</sub> = 1V	--	1	--	μA
Soft-Start Period		t <sub>SS</sub>		--	1	--	ms
Thermal Shutdown		T <sub>SD</sub>		--	150	--	°C
Thermal Shutdown Hysteresis		ΔT <sub>SD</sub>		--	15	--	°C
Power Good Threshold Rising				--	0.7	--	V
Power Good Threshold Hysteresis				--	130	--	mV
Power Good Pull Down Resistance				--	12	--	Ω
Output OVP Threshold				--	125	--	%V <sub>REF</sub>
Output OVP Propagation Delay				--	10	--	μs

**Note 1.** Stresses beyond those listed under “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

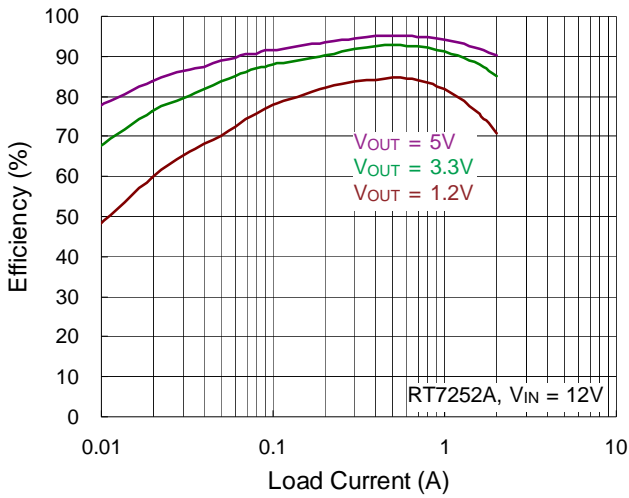
**Note 2.** θ<sub>JA</sub> is measured at T<sub>A</sub> = 25°C on a high effective thermal conductivity four-layer test board per JEDEC 51-7. θ<sub>JC</sub> is measured at the exposed pad of the package.

**Note 3.** Devices are ESD sensitive. Handling precaution is recommended.

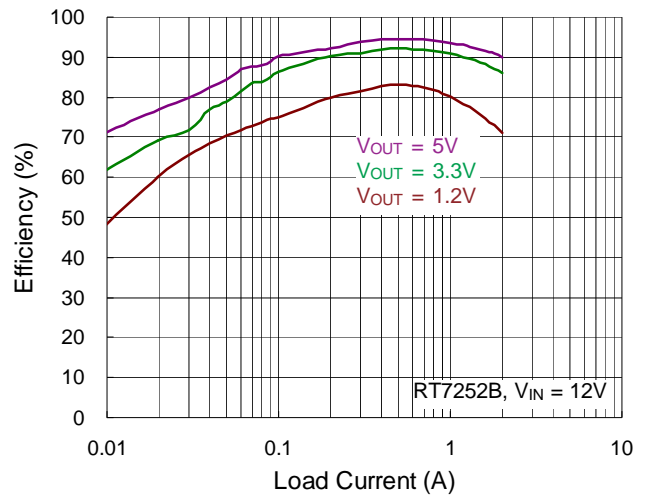
**Note 4.** The device is not guaranteed to function outside its operating conditions.

Typical Operating Characteristics

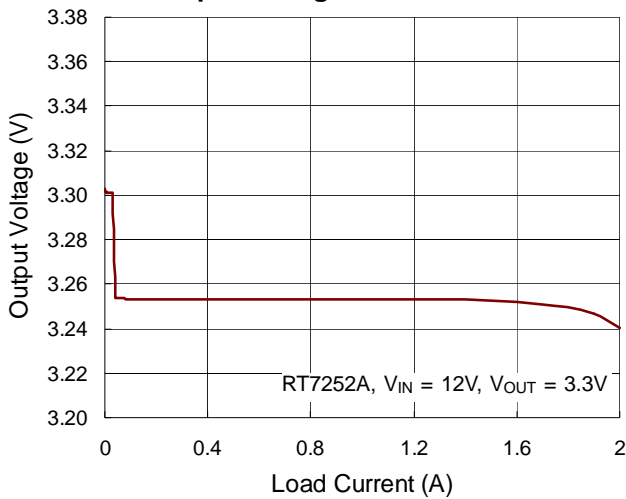
Efficiency vs. Load Current



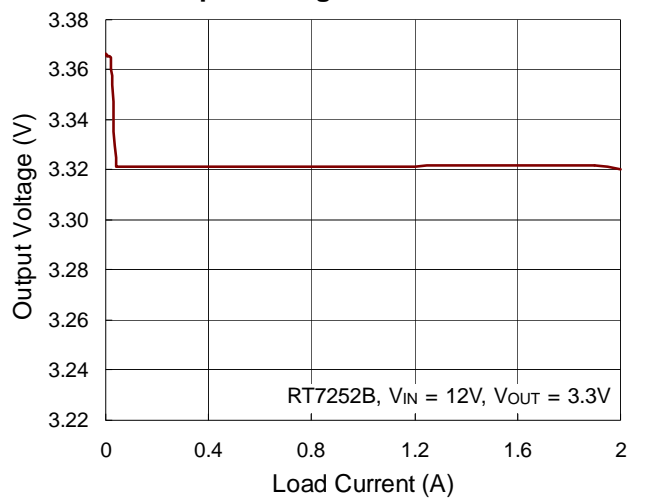
Efficiency vs. Load Current



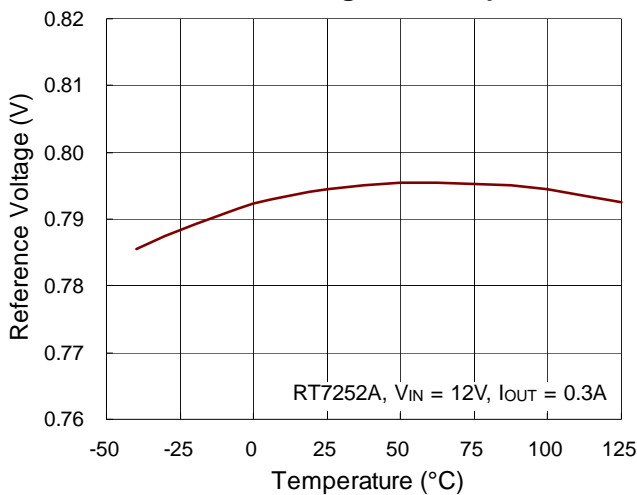
Output Voltage vs. Load Current



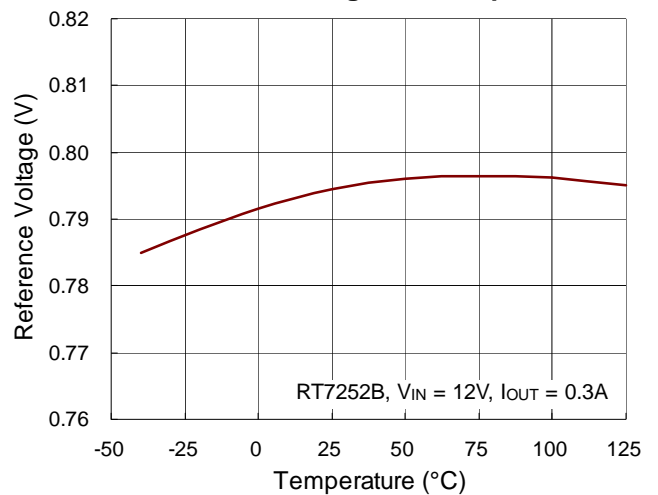
Output Voltage vs. Load Current



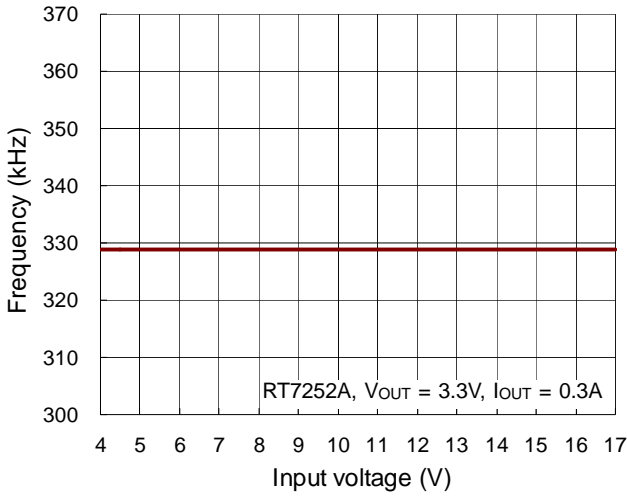
Reference Voltage vs. Temperature



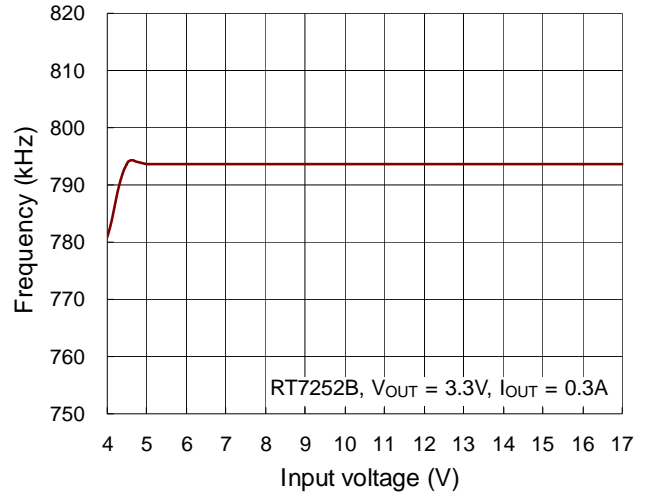
Reference Voltage vs. Temperature



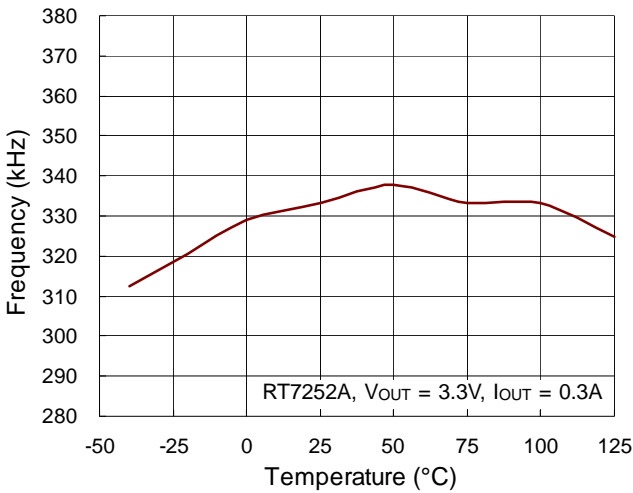
**Frequency vs. Input Voltage**



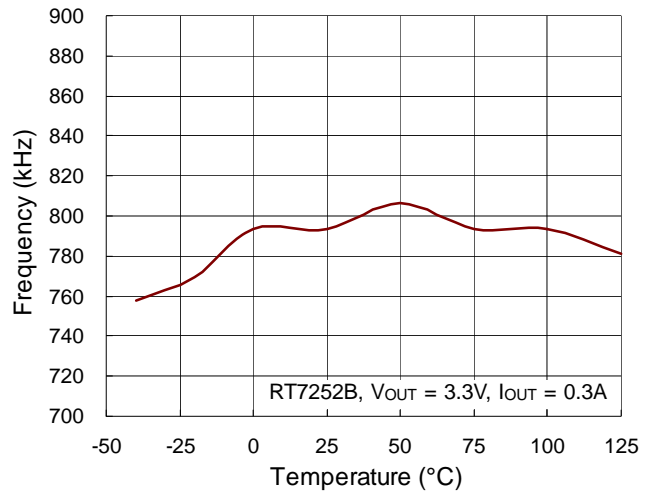
**Frequency vs. Input Voltage**



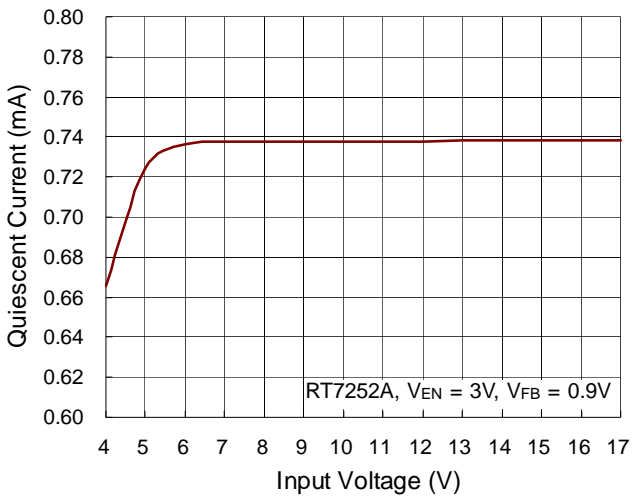
**Frequency vs. Temperature**



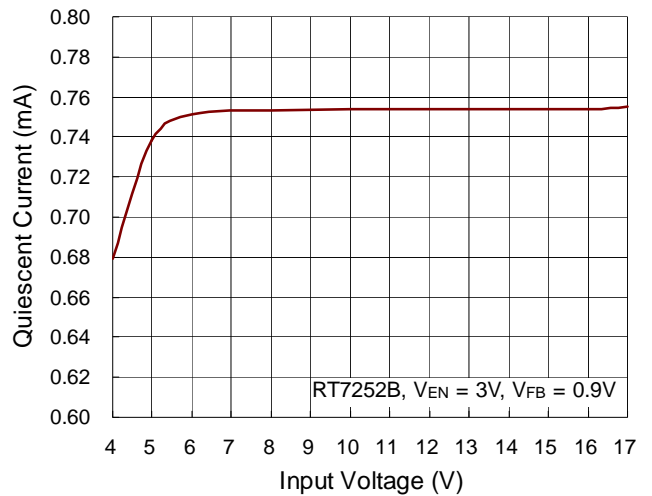
**Frequency vs. Temperature**

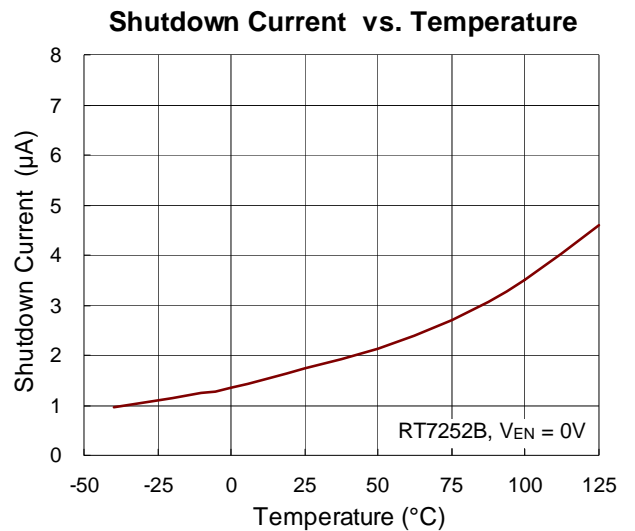
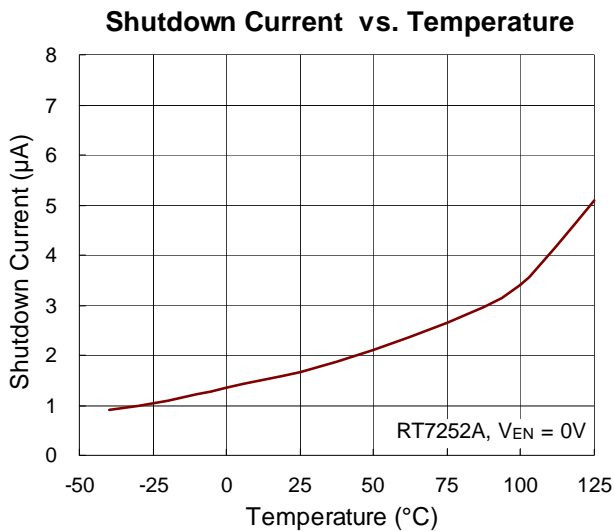
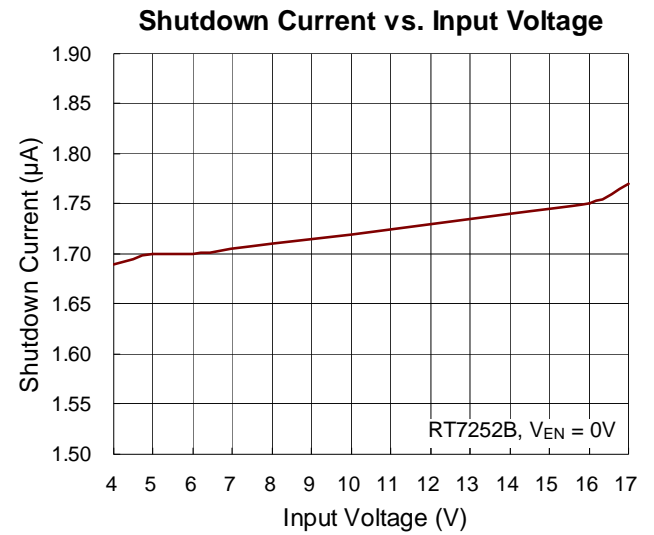
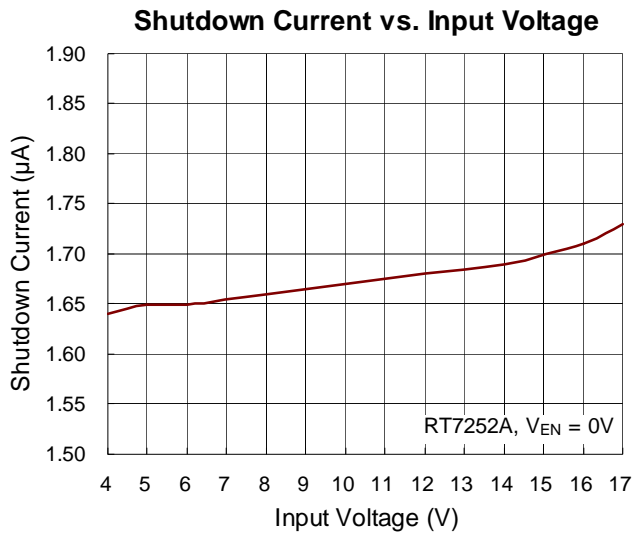
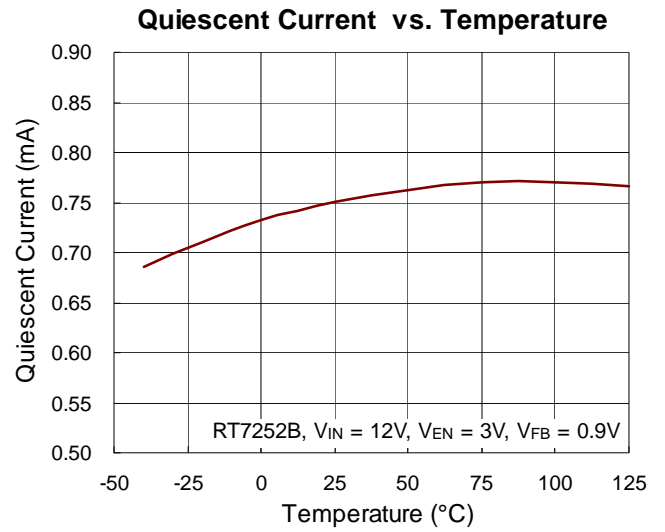
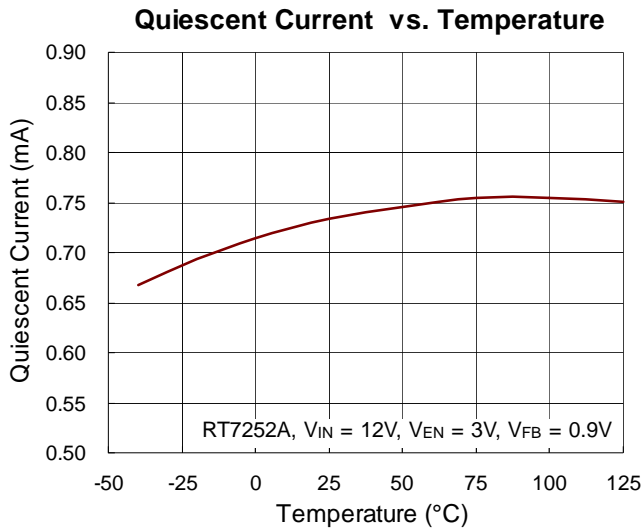


**Quiescent Current vs. Input Voltage**



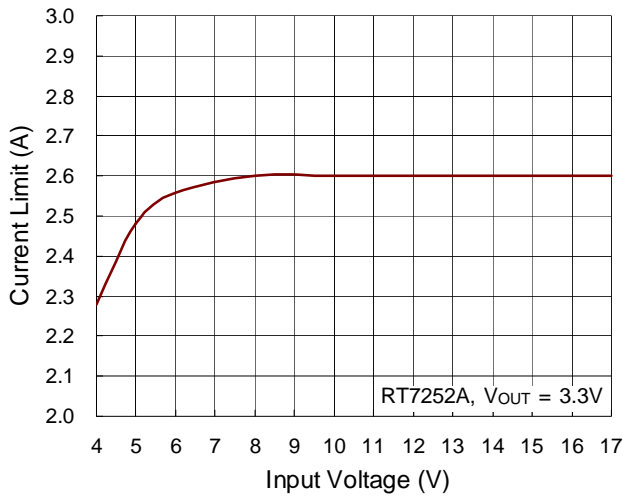
**Quiescent Current vs. Input Voltage**



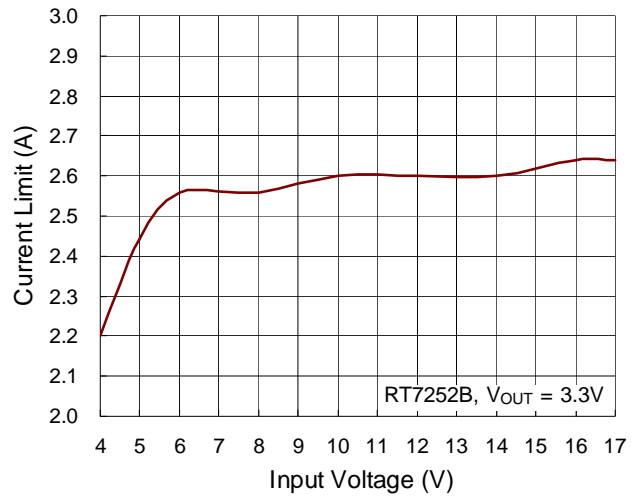




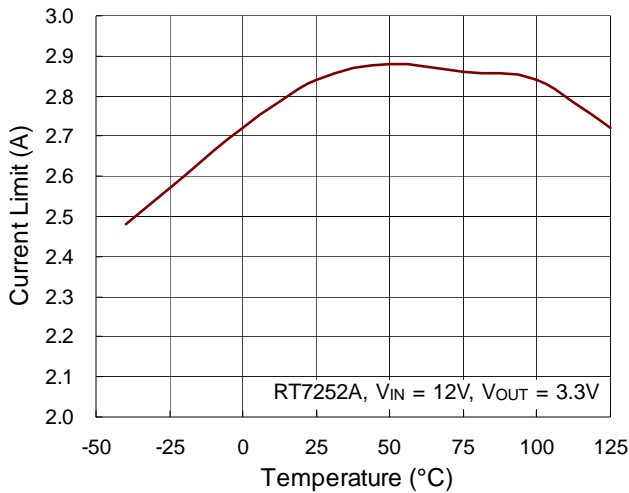
**Current Limit vs. Input Voltage**



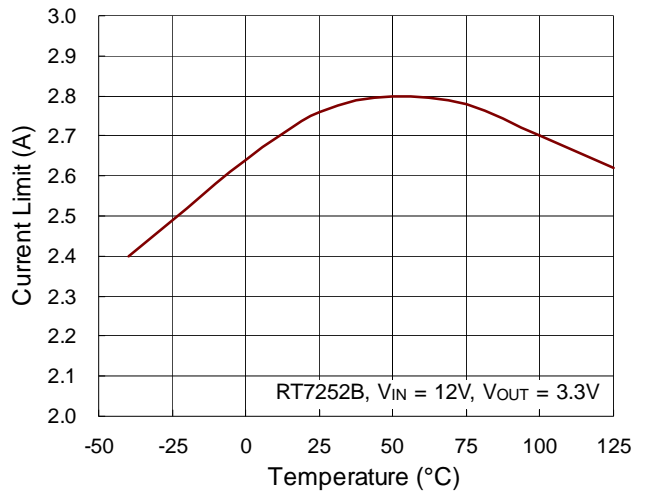
**Current Limit vs. Input Voltage**



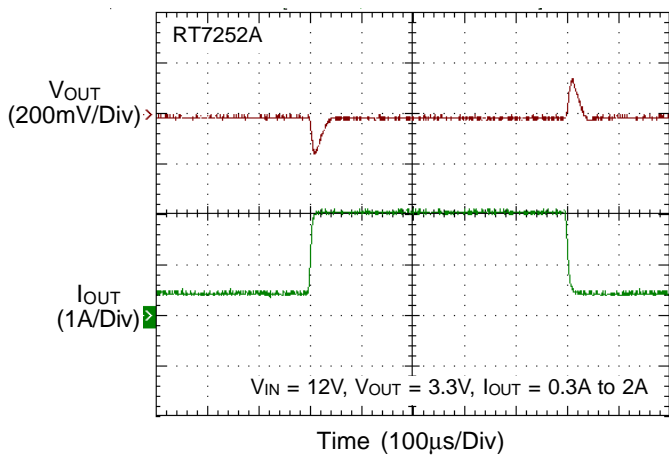
**Current Limit vs. Temperature**



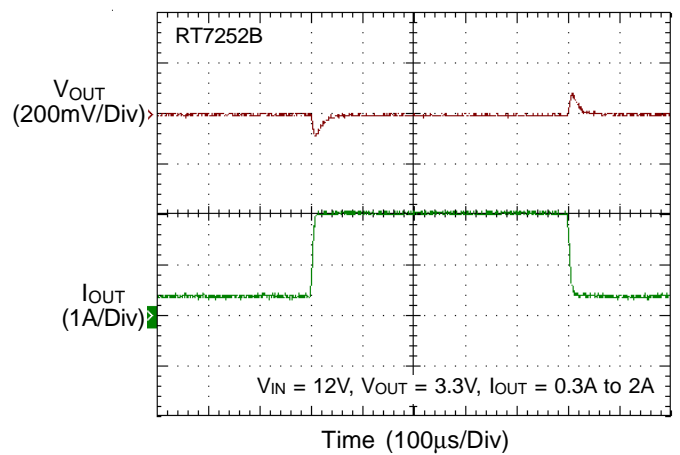
**Current Limit vs. Temperature**



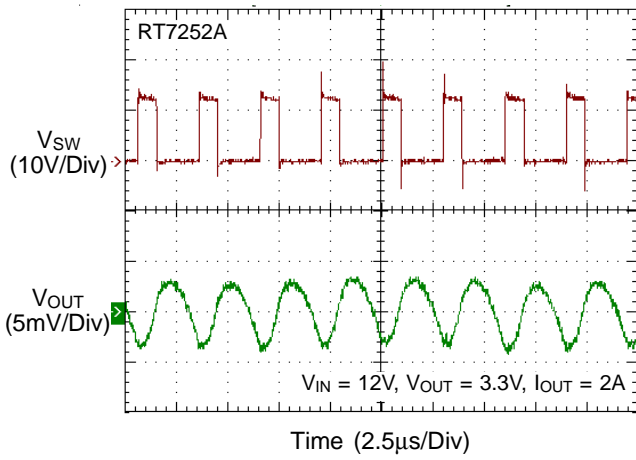
**Load Transient Response**



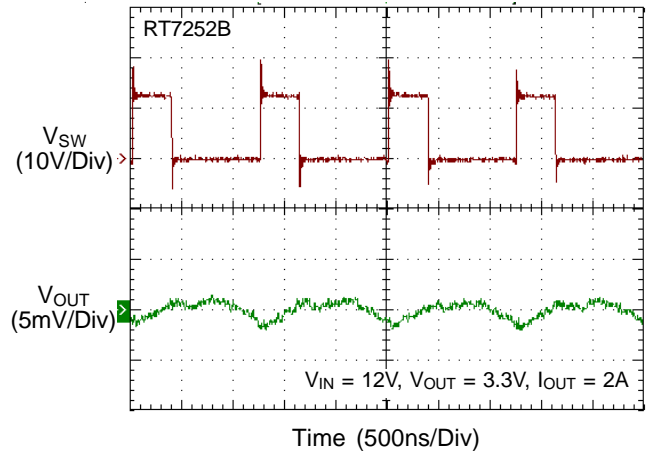
**Load Transient Response**



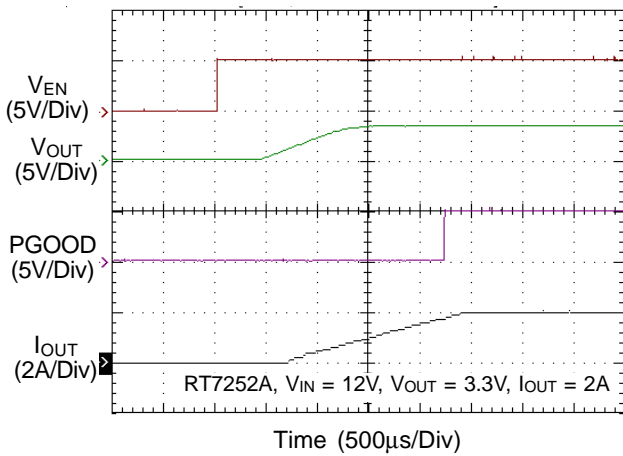
Switching



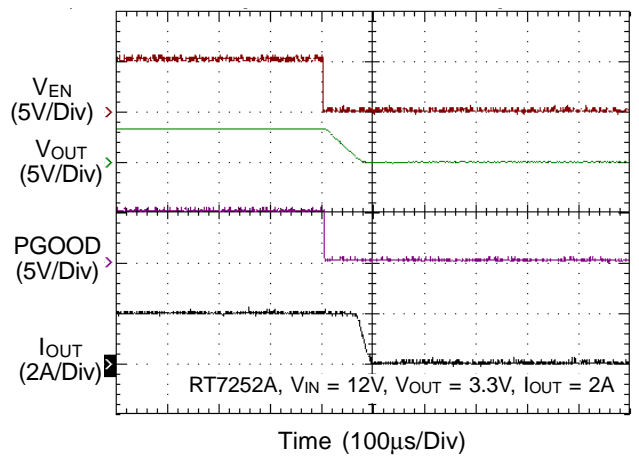
Switching



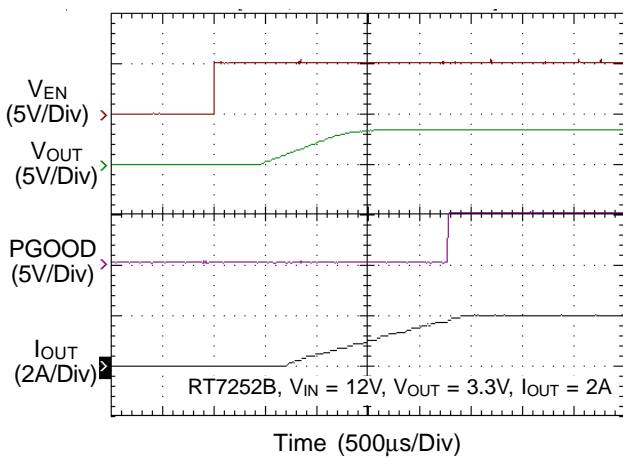
Power On from EN



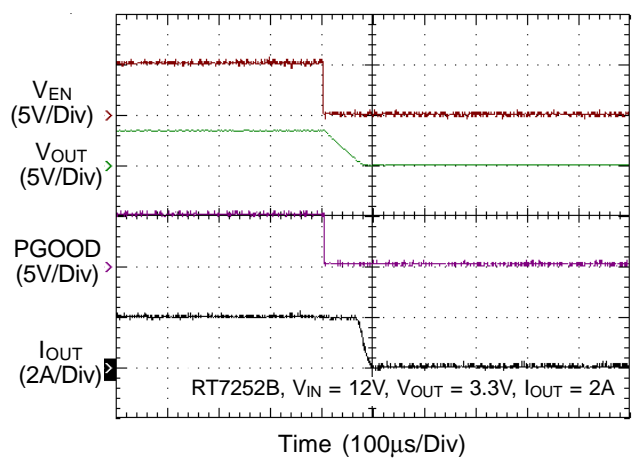
Power Off from EN



Power On from EN



Power Off from EN



## Application Information

The RT7252A/B is a synchronous high voltage buck converter that can support the input voltage range from 4V to 17V and the output current can be up to 2A.

### Output Voltage Setting

The resistive divider allows the FB pin to sense the output voltage as shown in Figure 1.

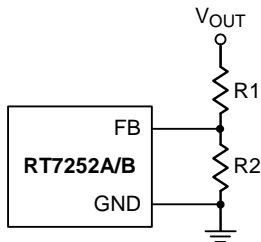


Figure 1. Output Voltage Setting

The output voltage is set by an external resistive divider according to the following equation :

$$V_{OUT} = V_{FB} \left( 1 + \frac{R1}{R2} \right)$$

where  $V_{FB}$  is the feedback reference voltage (0.8V typ.).

### External Bootstrap Diode

Connect a 10nF low ESR ceramic capacitor between the BOOT pin and SW pin. This capacitor provides the gate driver voltage for the high side MOSFET. It is recommended to add an external bootstrap diode between an external 5V and the BOOT pin for efficiency improvement when input voltage is lower than 5.5V or duty ratio is higher than 65%. The bootstrap diode can be a low cost one such as 1N4148 or BAT54. The external 5V can be a 5V fixed input from system or a 5V output of the RT7252A/B. Note that the external boot voltage must be lower than 5.5V

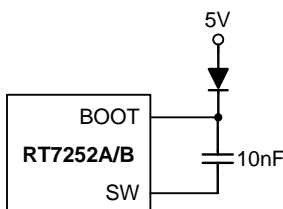


Figure 2. External Bootstrap Diode

### Over Voltage Protection (OVP)

The RT7252A/B provides over voltage protection function when output voltage is over 125%. The internal MOS will be turned off. The control will return to normal operation if over voltage condition is removed.

### Under Voltage Protection (UVP)

#### Latch-Off Mode

For the RT7252A/B, it provides Hiccup Mode Under Voltage Protection (UVP). When the FB voltage drops below 50% of the feedback reference voltage,  $V_{FB}$ , the UVP function will be triggered and the RT7252A/B will shut down for a period of time and then recover automatically. The Hiccup Mode UVP can reduce input current in short-circuit conditions.

### Inductor Selection

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_L = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. High frequency with small ripple current can achieve the highest efficiency operation. However, it requires a large inductor to achieve this goal. For the ripple current selection, the value of  $\Delta I_L = 0.2(I_{MAX})$  will be a reasonable starting point. The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[ \frac{V_{OUT}}{f \times \Delta I_L(MAX)} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

**Table 2. Suggested Inductors for Typical Application Circuit**

Component Supplier	Series	Dimensions (mm)
TDK	VLF10045	10 x 9.7 x 4.5
TDK	SLF12565	12.5 x 12.5 x 6.5
TAIYO YUDEN	NR8040	8 x 8 x 4

## C<sub>IN</sub> and C<sub>OUT</sub> Selection

The input capacitance, C<sub>IN</sub>, is needed to filter the trapezoidal current at the source of the high side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at V<sub>IN</sub> = 2V<sub>OUT</sub>, where I<sub>RMS</sub> = I<sub>OUT</sub>/2. This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design. For the input capacitor, a 10μF low ESR ceramic capacitor is recommended. For the recommended capacitor, please refer to table 3 for more details. The selection of C<sub>OUT</sub> is determined by the required ESR to minimize voltage ripple. Moreover, the amount of bulk capacitance is also a key for C<sub>OUT</sub> selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section. The output ripple, ΔV<sub>OUT</sub>, is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple will be highest at the maximum input voltage since ΔI<sub>L</sub> increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR value. However, it provides lower capacitance density than other types. Although Tantalum capacitors have the highest capacitance density, it is important to only use types that pass the surge test for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR. However, it can be used in cost-sensitive applications for ripple current rating and long term reliability considerations. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient

and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input, V<sub>IN</sub>. At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at V<sub>IN</sub> large enough to damage the part.

## Checking Transient Response

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs, V<sub>OUT</sub> immediately shifts by an amount equal to ΔI<sub>LOAD</sub> (ESR) also begins to charge or discharge C<sub>OUT</sub> generating a feedback error signal for the regulator to return V<sub>OUT</sub> to its steady-state value. During this recovery time, V<sub>OUT</sub> can be monitored for overshoot or ringing that would indicate a stability problem.

## Thermal Considerations

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where T<sub>J(MAX)</sub> is the maximum junction temperature, T<sub>A</sub> is the ambient temperature, and θ<sub>JA</sub> is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125°C. The junction to ambient thermal resistance,  $\theta_{JA}$ , is layout dependent. For SOP-8 (Exposed Pad) package, the thermal resistance,  $\theta_{JA}$ , is 75°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at  $T_A = 25^\circ\text{C}$  can be calculated by the following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (75^\circ\text{C/W}) = 1.333\text{W for SOP-8 (Exposed Pad) package}$$

The maximum power dissipation depends on the operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance,  $\theta_{JA}$ . The derating curve in Figure 3 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

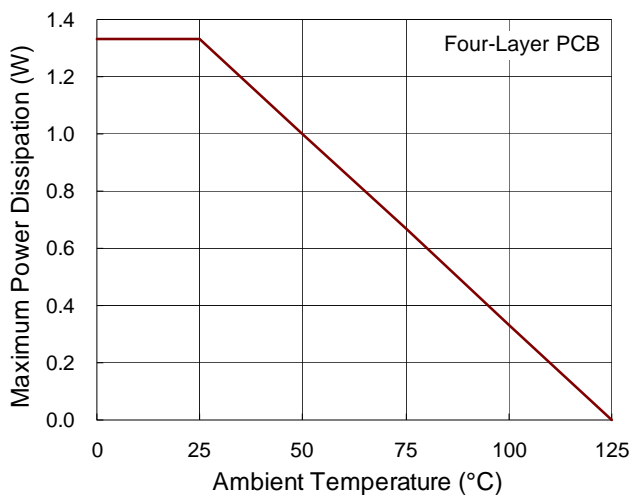


Figure 3. Derating Curve of Maximum Power Dissipation

**Layout Consideration**

Follow the PCB layout guidelines for optimal performance of the RT7252A/B

- ▶ Keep the traces of the main current paths as short and wide as possible.
- ▶ Put the input capacitor as close as possible to the device pins (VIN and GND).
- ▶ SW node is with high frequency voltage swing and should be kept at small area. Keep sensitive components away from the SW node to prevent stray capacitive noise pickup.
- ▶ Place the feedback components to the FB pin as close as possible.
- ▶ The GND and Exposed Pad should be connected to a strong ground plane for heat sinking and noise protection.

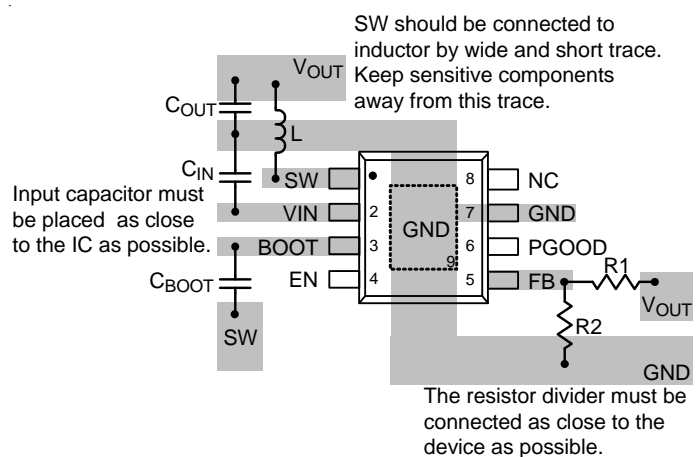
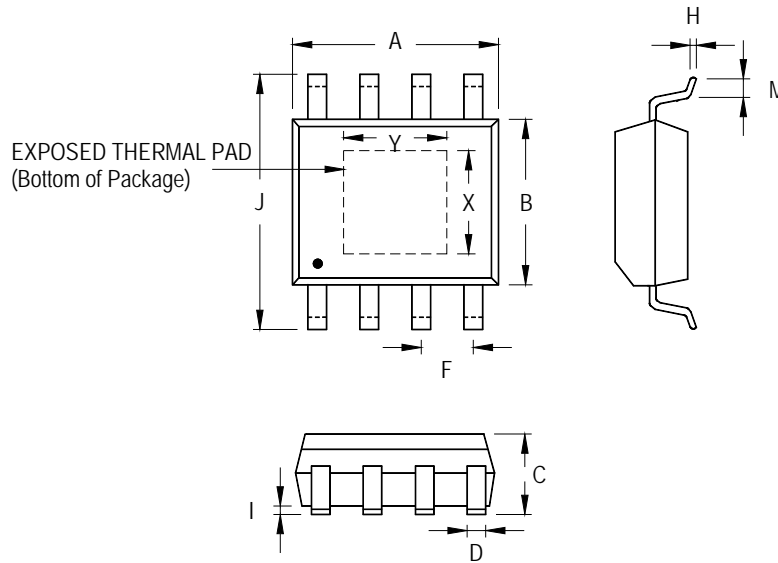


Figure 4. PCB Layout Guide

**Table 3. Suggested Capacitors for  $C_{IN}$  and  $C_{OUT}$**

Location	Component Supplier	Part No.	Capacitance ( $\mu\text{F}$ )	Case Size
$C_{IN}$	MURATA	GRM31CR61E106K	10	1206
$C_{IN}$	TDK	C3225X5R1E106K	10	1206
$C_{IN}$	TAIYO YUDEN	TMK316BJ106ML	10	1206
$C_{OUT}$	MURATA	GRM32ER61E226M	22	1210
$C_{OUT}$	MURATA	GRM21BR60J226M	22	0805
$C_{OUT}$	TDK	C3225X5R0J226M	22	1210
$C_{OUT}$	TAIYO YUDEN	EMK325BJ226MM	22	1210

Outline Dimension



Symbol	Dimensions In Millimeters		Dimensions In Inches		
	Min	Max	Min	Max	
A	4.801	5.004	0.189	0.197	
B	3.810	4.000	0.150	0.157	
C	1.346	1.753	0.053	0.069	
D	0.330	0.510	0.013	0.020	
F	1.194	1.346	0.047	0.053	
H	0.170	0.254	0.007	0.010	
I	0.000	0.152	0.000	0.006	
J	5.791	6.200	0.228	0.244	
M	0.406	1.270	0.016	0.050	
Option 1	X	2.000	2.300	0.079	0.091
	Y	2.000	2.300	0.079	0.091
Option 2	X	2.100	2.500	0.083	0.098
	Y	3.000	3.500	0.118	0.138

8-Lead SOP (Exposed Pad) Plastic Package

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